



Title	Work Output and Efficiency at Maximum Power of Linear Irreversible Heat Engines Operating with a Finite-Sized Heat Source
Author(s)	Izumida, Yuki; Okuda, Koji
Citation	Physical Review Letters, 112(18), 180603 https://doi.org/10.1103/PhysRevLett.112.180603
Issue Date	2014-05-08
Doc URL	http://hdl.handle.net/2115/56912
Rights	©2014 American Physical Society
Type	article
File Information	PhysRevLett_112_180603-.pdf



[Instructions for use](#)

Work Output and Efficiency at Maximum Power of Linear Irreversible Heat Engines Operating with a Finite-Sized Heat Source

Yuki Izumida¹ and Koji Okuda²

¹Department of Information Sciences, Ochanomizu University, Tokyo 112-8610, Japan

²Division of Physics, Hokkaido University, Sapporo 060-0810, Japan

(Received 22 September 2013; revised manuscript received 12 April 2014; published 8 May 2014)

We formulate the work output and efficiency for linear irreversible heat engines working between a finite-sized hot heat source and an infinite-sized cold heat reservoir until the total system reaches the final thermal equilibrium state with a uniform temperature. We prove that when the heat engines operate at the maximum power under the tight-coupling condition without heat leakage the work output is just half of the exergy, which is known as the maximum available work extracted from a heat source. As a consequence, the corresponding efficiency is also half of its quasistatic counterpart.

DOI: 10.1103/PhysRevLett.112.180603

PACS numbers: 05.70.Ln

Introduction.—Utilizing heat as the motive power has been an indispensable basis for our modern industrial society. The Carnot theorem is a cornerstone for heat-energy conversion, where a heat engine converts the heat Q_h into the work output W between the hot heat reservoir (source) at the temperature T_h and the cold heat reservoir (sink) at the temperature T_c ($T_c < T_h$). The theorem states that the efficiency $\eta = W/Q_h$ of the heat-energy conversion is bounded from above as

$$\eta \leq 1 - \frac{T_c}{T_h} \equiv \eta_C (\text{Carnot efficiency}), \quad (1)$$

showing that we need to discard a certain amount of heat $Q_c \equiv Q_h - W$ into the cold heat reservoir. Although the upper bound is achieved by reversible heat engines with infinitely slow (quasistatic) operation, such as in the Carnot cycle, the power (work output per unit time), which is another important performance criterion, vanishes in the quasistatic limit by definition. In this regard, for more practical relevance, the efficiency at maximum power η^* has been intensively studied [1–15].

In terms of practicality, it would also be relevant to consider the finiteness of the heat source. Even though the hot heat source may usually be treated as an infinite-sized heat reservoir in the thermodynamics of heat engines, it can actually be “fuel” as a finite resource with a finite amount of substance (e.g., burning coal in a steam engine) but not necessarily an infinite resource like the heat reservoir. This issue is becoming increasingly important due to the need for an urgent solution to the worldwide depletion of energy resources. To achieve a sustainable society, we need to consider this kind of fundamental thermodynamic limitation.

Reversible heat engines utilizing a finite-sized hot heat source have been considered in the context of exergy [16–19]. Exergy is the maximum available work defined as

the upper bound of the work output extracted from a finite-sized hot heat source until the hot heat source is brought to the final thermal equilibrium state sharing the same temperature as a cold heat reservoir (see the details below). The corresponding efficiency also achieves a maximum, but again, the power vanishes while the maximum work is extracted. Even though some previous literature addressed the available work extracted from a finite-sized heat source during finite-time operation and the corresponding efficiency [20–23], their results depended on phenomenological models with specific assumptions.

Our purpose is to formulate the work output and efficiency at the maximum power for linear irreversible heat engines working between a finite-sized hot heat source and an infinite-sized cold heat reservoir until the total system reaches the final thermal equilibrium state with a uniform temperature. Our theory is based on a general framework of linear irreversible thermodynamics [24,25]. We prove that, when the heat engines operate at the maximum power under the tight-coupling condition without heat leakage, the work output is just half of the exergy, and as a consequence, the corresponding efficiency is also half of its quasistatic counterpart. Our results also include $\eta^* = \eta_C/2$, obtained in [8] for linear irreversible heat engines working between two infinite-sized heat reservoirs under the tight-coupling condition as a special case.

Exergy.—The maximum work can be extracted by an energetically infinitesimal reversible heat engine between the temperatures T and T_c (e.g., the Carnot cycle), where T is the temperature of the hot heat source. Such a heat engine successively transforms the infinitesimal heat dQ_h into the infinitesimal work dW with the efficiency η^T at each T being the highest Carnot efficiency $\eta_C^T \equiv 1 - T_c/T$ until the temperature T of the hot heat source decreases from T_h to T_c [Fig. 1(a)]. The total work extracted by a heat engine from the finite-sized hot heat source defined by $W = \int dW = \int \eta^T dQ_h$ is bounded from above for the scenario in Fig. 1(a) as

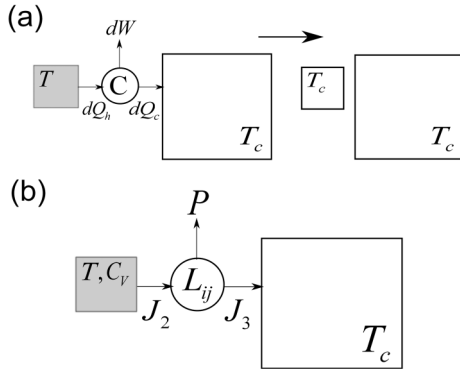


FIG. 1. (a) Energetically infinitesimal Carnot cycle working between a finite-sized hot heat source at a temperature T and the cold heat reservoir at the temperature T_c . The total system ends up in the final thermal equilibrium state sharing the uniform temperature T_c . (b) Linear irreversible heat engine working between a finite-sized hot heat source at T with a heat capacity at constant volume C_V and a cold heat reservoir at T_c .

$$W \leq \int \eta_C^T dQ_h = - \int_{T_h}^{T_c} \eta_C^T C_V dT = U_h - U_c - T_c(S_h - S_c) \equiv E, \quad (2)$$

where U_i (S_i) ($i = h, c$) are the internal energies (entropies) of the initial and final equilibrium states of the hot heat source using the definitions $U_h - U_c \equiv \int_{T_c}^{T_h} C_V dT$ and $S_h - S_c \equiv \int_{T_c}^{T_h} \frac{C_V}{T} dT$, with $C_V = C_V(T)$ denoting the heat capacity at constant volume of the hot heat source. This maximum work E is called the “exergy” [17]. Although the significance of the exergy is rarely considered in a context of physics (but see, e.g., [18,26]), it is a practically important concept that is often introduced in thermodynamics textbooks for engineers [19]. The exergy is not a state function since it depends on a condition under which the hot heat source supplies heat to the heat engine during the process. Although here we consider a constant-volume condition for simplicity, the concept of the exergy itself can also be considered for other thermodynamic conditions (e.g., a constant-pressure condition). The corresponding efficiency $\eta = W/Q_h = W/(U_h - U_c)$ is bounded from above as [27,28]

$$\eta \leq \frac{E}{U_h - U_c} = 1 - \frac{T_c(S_h - S_c)}{U_h - U_c} \equiv \eta_{\max}. \quad (3)$$

In the case that the hot heat source is a heat reservoir as $C_V \rightarrow \infty$, η_{\max} recovers the usual Carnot efficiency η_C by the definition $(U_h - U_c)/T_h = Q_h/T_h = S_h - S_c$ for an isothermal environment. Consequently, Eq. (3) for a finite-sized hot heat source is a generalization of the Carnot theorem in Eq. (1) for an infinite-sized hot heat source.

Linear irreversible thermodynamics framework.—The setup of our model is as follows [Fig. 1(b)]: consider a

linear irreversible heat engine [8] working between a finite-sized hot heat source and a cold heat reservoir at the temperature T_c . We assume that the hot heat source is always in an equilibrium state with a well-defined temperature T between T_c and T_h and the heat capacity at constant volume C_V . Initially at time $t = 0$, T is assumed to be T_h . We also assume that the heat engine successively transforms the heat (a small part of the internal energy of the hot heat source) into work at an efficiency depending on the working regime, and T continuously decreases from T_h to T_c accompanying the operation of the heat engine. We note that these assumptions could physically be realized under the two following relevant conditions: (i) the hot heat source rapidly relaxes to an equilibrium state with a well-defined temperature upon providing the heat energy to the heat engine, and (ii) the internal energy of the hot heat source is sufficiently larger than the amount of the heat energy supplied to the heat engine per cycle or unit time, which implies that it takes sufficiently many cycles or a long time to deplete the hot heat source.

The behavior of our heat engine during the process is described by linear irreversible thermodynamics, starting from consideration of the entropy production rate $\dot{\sigma}$ of the total system consisting of the heat engine, hot heat source, and cold heat reservoir. Here, the dot indicates a quantity per unit time or the derivative with respect to time. Because the internal state of the heat engine returns to the original state after a unit time for cyclic heat engines if the unit time is chosen as one cycle or remains unchanged for steady-state heat engines, we express $\dot{\sigma}$ only by the sum of the entropy increase rates of the hot heat source and cold heat reservoir as

$$\dot{\sigma} = -\frac{\dot{Q}_h}{T} + \frac{\dot{Q}_c}{T_c} = -\frac{\dot{W}}{T_c} + \dot{Q}_h \left(\frac{1}{T_c} - \frac{1}{T} \right). \quad (4)$$

Defining a generalized external force F that acts on its conjugate variable x , we write the power \dot{W} as $\dot{W} = -F\dot{x}$. Then, we naturally decompose $\dot{\sigma} = F\dot{x}/T_c + \dot{Q}_h(1/T_c - 1/T)$ as $\dot{\sigma} = J_1 X_1 + J_2 X_2$, defining the thermodynamic fluxes J_1 (the motion speed of the heat engine) and J_2 (the heat flux from the hot heat source) in response to their conjugate thermodynamic forces X_1 (the external force) and X_2 (the thermal gradient), respectively, as

$$X_1 \equiv \frac{F}{T_c}, \quad J_1 \equiv \dot{x}, \quad (5)$$

$$X_2 \equiv \frac{1}{T_c} - \frac{1}{T} = \frac{T - T_c}{TT_c}, \quad J_2 \equiv \dot{Q}_h. \quad (6)$$

We assume that these variables are related to the linear Onsager relations [8,24,25] as

$$J_1 = L_{11}X_1 + L_{12}X_2, \quad (7)$$

$$J_2 = L_{21}X_1 + L_{22}X_2, \quad (8)$$

where L_{ij} denotes the Onsager coefficients with the reciprocal relation $L_{12} = L_{21}$. We note that, from the nonnegativity of $\dot{\sigma} = J_1X_1 + J_2X_2 \geq 0$, the possible values of L_{ij} are restricted as

$$L_{11} \geq 0, \quad L_{22} \geq 0, \quad L_{11}L_{22} - L_{12}L_{21} \geq 0. \quad (9)$$

For a simpler formulation, we change the variable from X_1 to J_1 as $X_1 = (J_1 - L_{12}X_2)/L_{11}$ through Eq. (7) and replace the Onsager relations with J_2 and the heat flux to the cold heat reservoir $J_3 \equiv \dot{Q}_c = \dot{Q}_h - \dot{W} = J_2 + J_1X_1T_c$ [15]:

$$J_2 = \frac{L_{21}}{L_{11}}J_1 + L_{22}(1 - q^2)X_2, \quad (10)$$

$$J_3 = \frac{L_{21}T_c}{L_{11}T}J_1 + L_{22}(1 - q^2)X_2 + \frac{T_c}{L_{11}}J_1^2, \quad (11)$$

where q is the coefficient of the coupling strength defined as [29]

$$q \equiv \frac{L_{21}}{\sqrt{L_{11}L_{22}}}, \quad (|q| \leq 1). \quad (12)$$

The restriction of q comes from Eq. (9). Each term in Eqs. (10) and (11) has a clear physical interpretation [15]: the first terms in Eqs. (10) and (11) imply the reversible heat transfer from the hot heat source and that to the cold heat reservoir, which do not contribute to $\dot{\sigma}$ at all. The second terms in Eqs. (10) and (11) imply the heat leakage from the hot heat source to the cold heat reservoir with $L_{22}(1 - q^2)/TT_c$ being the thermal conductance, which remain irrespective of the operation of the heat engine with $|q| \neq 1$. The third term in Eq. (11) implies the dissipation into the cold heat reservoir accompanying the operation of the heat engine.

Under the condition $|q| = 1$ called ‘‘tight coupling,’’ the heat-leakage terms vanish, and the heat fluxes go to zero simultaneously in the quasistatic limit of $J_1 \rightarrow 0$. This idealized but most interesting condition can be realized, e.g., by a finite-time Carnot cycle [30].

The power $\dot{W} = J_2 - J_3$ is rewritten by using Eqs. (10) and (11) as

$$\dot{W} = \frac{L_{12}}{L_{11}}\eta_C^T J_1 - \frac{T_c}{L_{11}}J_1^2. \quad (13)$$

The decreasing rate of the temperature T of the hot heat source during the operation of the heat engine is given by

$$C_V \frac{dT}{dt} = C_V \dot{T} = -J_2, \quad (14)$$

where J_2 is given by Eq. (10). Equation (14) can also be considered as a relation that connects the temperature T to the time t . Although J_i , X_i , L_{ij} , and C_V may depend on T [or t through Eq. (14)] in general, we write the T dependence explicitly only when we stress it. Equations (10) and (11) together with Eq. (14) constitute the time-evolution equations of $T(t)$ for a given working regime $J_1(t)$.

After these preparations, we consider the work output and efficiency of this system. The heat from the hot heat source Q_h and the work output W between the initial time $t = 0$ and the final time $t = \tau$ are given as

$$Q_h = \int_0^\tau J_2(t)dt = - \int_{T_h}^{T_c} C_V dT = U_h - U_c, \quad (15)$$

$$W = \int_0^\tau \dot{W}(t)dt = U_h - U_c - \int_0^\tau J_3(t)dt, \quad (16)$$

respectively, where we used Eq. (14), $T(0) = T_h$, and $T(\tau) = T_c$. W is a functional of J_1 [or equivalently T through Eq. (14)] via J_3 in Eq. (11). We also express the total power P and the efficiency η as

$$P = \frac{W}{\tau} = \frac{U_h - U_c - \int_0^\tau J_3(t)dt}{\tau}, \quad (17)$$

$$\eta = \frac{W}{Q_h} = 1 - \frac{\int_0^\tau J_3(t)dt}{U_h - U_c}, \quad (18)$$

respectively.

Main results.—We maximize Eq. (17) by first minimizing the integral $\int_0^\tau J_3(t)dt$ in Eq. (17) under the fixed time τ and then maximizing $P(\tau)$ as follows. By solving Eq. (14) with respect to J_1 , we express $J_1(t)$ as a function of T and \dot{T} as

$$J_1(T, \dot{T}) = -\frac{L_{11}}{L_{21}}C_V \dot{T} - \frac{L_{11}L_{22}(1 - q^2)}{L_{21}}X_2. \quad (19)$$

Then we express the integrand $J_3(t) = J_3(T, \dot{T})$ as

$$J_3(T, \dot{T}) = -T_c C_V \frac{\dot{T}}{T} + \frac{L_{22}(1 - q^2)X_2^2 T_c}{q^2} + \frac{T_c C_V^2 \dot{T}^2}{q^2 L_{22}} + \frac{2T_c}{q^2} C_V \dot{T}(1 - q^2)X_2 \quad (20)$$

by substituting $J_1(T, \dot{T})$ into Eq. (11). We minimize the integral $\int_0^\tau J_3(T, \dot{T})dt$ in Eq. (17) by solving the following Euler-Lagrange (EL) equation for $T(t)$:

$$\frac{d}{dt} \left(\frac{\partial J_3(T, \dot{T})}{\partial \dot{T}} \right) - \frac{\partial J_3(T, \dot{T})}{\partial T} = 0. \quad (21)$$

By substituting Eq. (20) into Eq. (21), we obtain the EL equation to be solved as

$$\frac{2C_V^2}{q^2 L_{22}} \ddot{T} + \dot{T}^2 \frac{\partial}{\partial T} \left(\frac{C_V^2}{q^2 L_{22}} \right) - \frac{\partial}{\partial T} \left(\frac{L_{22}(1-q^2)X_2^2}{q^2} \right) = 0. \quad (22)$$

Note that C_V , L_{22} , and q may depend on T . By multiplying both sides by \dot{T} , Eq. (22) is simplified to

$$\frac{d}{dt} \left(\frac{C_V^2}{q^2 L_{22}} \dot{T}^2 - \frac{L_{22}(1-q^2)X_2^2}{q^2} \right) = 0. \quad (23)$$

It may be difficult to find an explicit form of the general solution of $T(t)$ from Eq. (23).

However, under the tight-coupling condition $|q| = 1$, which is idealized but is the most interesting condition, we can calculate the integral $\int_0^\tau J_3(T, \dot{T}) dt$ by utilizing Eq. (23) without solving it explicitly as follows. By integrating Eq. (23), we obtain

$$\frac{C_V}{\sqrt{L_{22}}} \dot{T} = A(\text{integral const}). \quad (24)$$

By integrating Eq. (24) from $t = 0$ to $t = \tau$, we obtain

$$A = \frac{\int_{T_h}^{T_c} \frac{C_V}{\sqrt{L_{22}}} dT}{\tau} \equiv \frac{B}{\tau}, \quad (25)$$

where B is a constant independent of τ . By using Eqs. (20), (24), and (25), we calculate the integral $\int_0^\tau J_3(T, \dot{T}) dt$ and the total power in Eq. (17) as

$$\begin{aligned} \int_0^\tau J_3 dt &= -T_c \int_0^\tau \left(\frac{C_V \dot{T}}{T} - A^2 \right) dt \\ &= T_c(S_h - S_c) + \frac{T_c B^2}{\tau}, \end{aligned} \quad (26)$$

$$P_{|q|=1} = \frac{E}{\tau} - \frac{T_c B^2}{\tau^2}, \quad (27)$$

respectively. Note that $\eta_{|q|=1}$ in Eq. (18) $\rightarrow \eta_{\max}$ in Eq. (3) and $P_{|q|=1} \rightarrow 0$ in the quasistatic limit $\tau \rightarrow \infty$.

By maximizing Eq. (27) with respect to τ , we obtain the maximum power as

$$P_{|q|=1}^* = \frac{E^2}{4T_c B^2} \left(\text{at } \tau^* = \frac{2T_c B^2}{E} \right). \quad (28)$$

Using Eq. (28), we finally obtain the work output at the maximum power under the tight-coupling condition as

$$W_{|q|=1}^* = P_{|q|=1}^* \tau^* = \frac{E}{2}, \quad (29)$$

which is just half of the exergy. Then, as a consequence of Eq. (29), we also conclude that the efficiency at the maximum power under the tight-coupling condition $\eta_{|q|=1}^*$ is also half of the maximum efficiency in Eq. (3) as

$$\eta_{|q|=1}^* = \frac{W_{|q|=1}^*}{U_h - U_c} = \frac{1}{2} \eta_{\max}. \quad (30)$$

We note that in the case where the hot heat source is a hot heat reservoir as $C_V \rightarrow \infty$, $\eta_{|q|=1}^*$ in Eq. (30) recovers $\eta_C/2$, as previously derived for the linear irreversible heat engines working between the heat reservoirs [8]. Although we considered only the tight-coupling case, it is quite natural to expect that Eqs. (29) and (30) also serve as the *upper bounds* for the work output and efficiency at the maximum power, respectively, as the heat-leakage terms in Eqs. (10) and (11) do not contribute to the work output at all but just reduce the available internal energy of the hot heat source. This would also be consistent with the fact that the tight-coupling case serves as the upper bound of the efficiency at the maximum power η^* for linear irreversible heat engines with the infinite-sized heat reservoir $C_V \rightarrow \infty$ as in Eq. (9) of [8] because our theory should also lead to Eq. (9) of [8] in that limit.

Concluding remarks.—We formulated the work output and efficiency for linear irreversible heat engines working between a finite-sized hot heat source and an infinite-sized cold heat reservoir until the total system reaches the final thermal equilibrium state with a uniform temperature. We proved that, when the heat engines operate at the maximum power under the tight-coupling condition without heat leakage, the work output is just half of the exergy reached at the quasistatic limit, and as a consequence, the corresponding efficiency is also half of its quasistatic counterpart. Because our results can be applied to any type of working substance and do not assume any specific form of the Onsager coefficients and the heat capacity, we expect that they are universal, as are Eqs. (2) and (3) derived by equilibrium thermodynamics.

Finally, we remark on some possible extensions of the present study. First, further extension of our formulation to systems operating with a finite-sized cold heat sink instead of a cold heat reservoir [20,21,28] is straightforward. Second, the idea presented here could naturally be applied to other types of heat devices such as refrigerators and heat pumps [31–33] because their original function is cooling or heating a system to a desirable temperature [32,33], where the system should be regarded as a finite-sized heat source or sink. Third, an extension to nonlinear response regimes [10–15] would also be a challenging task for possible future studies. Fourth, seeing that optimization of fluctuating nano- and micron-sized heat engines has become a hot

topic with recent technological advances [34–36], we are naturally motivated to apply the exergetic concept to these systems. In relation to this, it is also interesting that a nonequilibrium equality such as the Crooks fluctuation theorem [37] has also been extended to a finite-sized heat reservoir [38]. Fifth, we stress that our theory could serve as a “zeroth approximation” for a possible future theory describing heat engines with a far-from-equilibrium heat source, such as a steam engine powered by burning coal.

We expect that the present work not only expands the scope of finite-time thermodynamics but also provides a design principle and an operational scheme for actual thermodynamic devices and power plants for a sustainable society.

Y. I. acknowledges the financial support from a Grant-in-Aid for JSPS Fellows (Grant No. 25-9748). The authors thank A. Calvo Hernández for useful comments on the manuscript.

-
- [1] F. Curzon and B. Ahlborn, *Am. J. Phys.* **43**, 22 (1975).
 [2] J. Yvon, in *Proceedings of the International Conference on Peaceful Uses of Atomic Energy* (United Nations, Geneva, 1955), Vol. 2, p. 337.
 [3] I. I. Novikov, *J. Nucl. Energy* **7**, 125 (1958).
 [4] P. T. Landsberg and H. S. Leff, *J. Phys. A* **22**, 4019 (1989).
 [5] J. M. Gordon, *Am. J. Phys.* **57**, 1136 (1989).
 [6] A. Benjamin, *J. Appl. Phys.* **79**, 1191 (1996).
 [7] P. Salamon, J. D. Nulton, G. Siragusa, T. R. Andersen, and A. Limon, *Energy* **26**, 307 (2001).
 [8] C. Van den Broeck, *Phys. Rev. Lett.* **95**, 190602 (2005).
 [9] B. Jiménez de Cisneros and A. Calvo Hernández, *Phys. Rev. Lett.* **98**, 130602 (2007).
 [10] M. Esposito, K. Lindenberg, and C. Van den Broeck, *Phys. Rev. Lett.* **102**, 130602 (2009).
 [11] T. Schmiedl and U. Seifert, *Europhys. Lett.* **81**, 20003 (2008).
 [12] B. Gaveau, M. Moreau, and L. S. Schulman, *Phys. Rev. Lett.* **105**, 060601 (2010).
 [13] M. Esposito, R. Kawai, K. Lindenberg, and C. Van den Broeck, *Phys. Rev. Lett.* **105**, 150603 (2010).
 [14] U. Seifert, *Phys. Rev. Lett.* **106**, 020601 (2011).
 [15] Y. Izumida and K. Okuda, *Europhys. Lett.* **97**, 10004 (2012).
 [16] J. W. Gibbs, *Transactions of the Connecticut Academy of Arts and Sciences* **2**, 382 (1873), reprinted in *The Scientific Papers of J. Willard Gibbs* (Dover, New York, 1961), Vol. 1, p. 33.
 [17] Z. Rant, *Forschung auf dem Gebiete des Ingenieurwesens* **22**, 36 (1956).
 [18] H. Callen, *Thermodynamics and an Introduction to Thermostatistics* (Wiley, New York, 1985), 2nd ed., Chap. 4.
 [19] M. J. Moran, H. N. Shapiro, D. D. Boettner, and M. B. Bailey, *Fundamentals of Engineering Thermodynamics* (Wiley, New York, 2010), 7th ed., Chap. 7.
 [20] Z. Yan and L. Chen, *J. Phys. A* **30**, 8119 (1997).
 [21] M. J. Ondrechen, M. H. Rubin, and Y. B. Band, *J. Chem. Phys.* **78**, 4721 (1983).
 [22] B. Andresen, M. H. Rubin, and R. S. Berry, *J. Phys. Chem.* **87**, 2704 (1983).
 [23] B. Andresen, R. S. Berry, M. J. Ondrechen, and P. Salamon, *Acc. Chem. Res.* **17**, 266 (1984).
 [24] L. Onsager, *Phys. Rev.* **37**, 405 (1931).
 [25] S. R. de Groot and P. Mazur, *Non-Equilibrium Thermodynamics* (Dover, New York, 1984).
 [26] S. Deffner and E. Lutz, *Phys. Rev. Lett.* **107**, 140404 (2011).
 [27] M. J. Ondrechen, B. Andresen, M. Mozurkewich, and R. S. Berry, *Am. J. Phys.* **49**, 681 (1981).
 [28] H. S. Leff, *Am. J. Phys.* **55**, 701 (1987).
 [29] O. Kedem and S. R. Caplan, *Trans. Faraday Soc.* **61**, 1897 (1965).
 [30] Y. Izumida and K. Okuda, *Phys. Rev. E* **80**, 021121 (2009).
 [31] B. Jiménez de Cisneros, L. A. Arias-Hernández, and A. Calvo Hernández, *Phys. Rev. E* **73**, 057103 (2006).
 [32] C. Van den Broeck and R. Kawai, *Phys. Rev. Lett.* **96**, 210601 (2006).
 [33] M. van den Broek and C. Van den Broeck, *Phys. Rev. Lett.* **100**, 130601 (2008).
 [34] O. Abah, J. Roßnagel, G. Jacob, S. Deffner, F. Schmidt-Kaler, K. Singer, and E. Lutz, *Phys. Rev. Lett.* **109**, 203006 (2012).
 [35] J. Roßnagel, O. Abah, F. Schmidt-Kaler, K. Singer, and E. Lutz, *Phys. Rev. Lett.* **112**, 030602 (2014).
 [36] V. Blickle and C. Bechinger, *Nat. Phys.* **8**, 143 (2012).
 [37] G. E. Crooks, *Phys. Rev. E* **60**, 2721 (1999).
 [38] M. Campisi, P. Talkner, and P. Hänggi, *Phys. Rev. E* **80**, 031145 (2009).